Comprehensive condition assessment program on the fire damaged structure – a project case in Singapore

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AGENDA

1. General Background
2. Literature Review
3. Condition Assessment
4. Analysis
5. Conclusion
1. GENERAL BACKGROUND

- Fire incident at construction site in the Eastern Part of Singapore
1. GENERAL BACKGROUND

Some concrete spalling exposing corroded steel reinforcements were noted on the roof level post tensioned beam and reinforced concrete slab.
1. GENERAL BACKGROUND

- The objective of the works was to **evaluate the condition** of the affected structure and the **residual material mechanical properties**.
- To determine the most effective structural rehabilitation program, which includes structural repair and strengthening works, further to this condition assessment, a complete structural assessment was performed.
2. LITERATURE REVIEW

- When exposed to high temperature, such as in the case of a fire, the concrete surface will become porous with lots of void and micro cracks.
- Some portion of the concrete may have shallow delamination, and some may even spall off.
- Porous concrete will reduce its compressive strength and increase the risk of rebar corrosion.
2. LITERATURE REVIEW

- The extent of concrete damage, such as carbonation depth, the existence of void and micro cracks, and estimation of concrete temperature during a fire, can be examined using Petrographic Examination on the concrete core sample [ASTM C856-04].

- Although the concrete surface may look to be in a good condition, with no crack and spalling, some internal separation (delamination) may occur, which is quite dangerous if not properly assessed. Structural repairs are required for this area to prevent concrete spalling in the future. Acoustic impact testing was used to detect the concrete area with shallow delamination [ASTM D4580].

- The residual concrete compressive strength might be the most important thing to be assessed to ensure the affected structures still have the required capacity to take the load. The compressive test was conducted on the extracted core samples [BS 1881: Part 120].
2. LITERATURE REVIEW

• It would be difficult to assess the extent of damage the fire caused to the structure unless a lot of samples are taken. To minimize the number of samples, a material uniformity test is required. This can be done using the Rebound Hammer test on the accessible concrete surface [ASTM C805]. Once the test showed that the readings of the material were not uniform, more samples would be required.
2. LITERATURE REVIEW

- After the fire reached a certain temperature, the steel mechanical properties, including its tensile strength, ductility, and hardness will change. The tensile strength test is required to determine the residual strength of the steel rebar to ensure that it has the required strength as per design requirement. Steel bend test is one method to qualitatively evaluate ductility. Vickers hardness test is used to evaluate the steel rebar hardness.
Petrographic Examination

- Petrographic Examination was performed in accordance to ASTM C856-04 on a ground section using a stereo microscope and on a thin section with a polarizing and fluorescent microscope (PFM), under transmitted and reflected light.

- Through an examination of the ground section, the assessment was made on the homogeneity of the concrete, compaction and types and distribution of large particles.

- Under transmitted light on the examination of a thin section, various components (type of cement and aggregates), air voids content, compaction pores and damage phenomenon in the sample were identified.

- Under reflected light, the fluorescent microscopy made it possible to study the homogeneity of the mix and the cement paste, capillary porosity, micro cracks and other defects in the sample.
2. LITERATURE REVIEW

**Acoustic Impact Testing**

- Using the principle of emission of elastic sound waves, the impacted surfaces exhibit either a sharp metallic ring or a dull hollow sound representing “sound” and “unsound” concrete conditions, respectively.
2. LITERATURE REVIEW

Steel Bend Test

• Steel bend test is one method to qualitatively evaluate ductility. It is done by bending the steel sample to a 45° angle and then heating it up to 100°C for at least 30 minutes. After it cools down the specimen is re-straightened to at least a 23° angle and it should not show any damage.

Steel Hardness Test [Vickers Hardness Test]

• Vickers hardness test is used to evaluate the steel rebar hardness. A constant force of 10kg is often used to obtain the Vickers Hardness Value (VH10), which can be indicatively correlated to give an estimation to its yield strength.
3. CONDITION ASSESSMENT

3.1. FIELD ASSESSMENT

- Soffit of Roof Level
- Top of 3rd Storey
- Concrete Core Sample Extraction for Compressive Strength Test
- Rebound Hammer Test
- Ferroscan Pachometer Survey
- Steel Rebar Sample Collection
- Concrete Core Sample Extraction for Petrographic Examination

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- Rebound Hammer Test
- Ferroscan Pachometer Survey
- Concrete Core Sample Extraction for Compressive Strength Test
- Concrete Core Sample Extraction for Petrographic Examination
- Steel Rebar Sample Collection
3. CONDITION ASSESSMENT

3.1. FIELD ASSESSMENT

3.1.1. Visual Inspection

- Accessible areas of the concrete structure were visually examined.
- Some concrete spalling exposing corroded steel reinforcements were noted on the roof storey beam and slab soffit.
- No sign of concrete defect was found on the 3rd storey beam and slab where the fire occurred.
- No damage was noted on the PT Tendon ducts, even at the most severely spalled concrete.

3.1.2. Acoustic Impact Testing

- Generally, unsound (i.e., delaminated) areas were in the immediate proximity of cracks in the beams. No concrete delamination was noted outside the spalled concrete area.
3. CONDITION ASSESSMENT

3.1. FIELD ASSESSMENT

3.1.3. Rebound Hammer Testing

- This method is not intended as an alternative for strength determination of concrete, but rather the scale number values provide qualitative comparisons between similar concrete materials.
- Typically, for each location, a series of 10 readings are performed approximately 25mm apart with test results recorded and tabulated.
- Eighteen (18) locations were tested with Rebound Hammer testing.
- Interpolating concrete strengths derived from Rebound Hammer manufacturer Data Charts, revealed a mean interpretative compressive strength of 30 - 50 N/mm$^2$. 
3. CONDITION ASSESSMENT

3.1. FIELD ASSESSMENT

3.1.3. Rebound Hammer Testing

<table>
<thead>
<tr>
<th>No</th>
<th>Location</th>
<th>Measurement</th>
<th>Interpretive $f_{cu}$ (N/mm$^2$)</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td></td>
<td>Low</td>
<td>High</td>
</tr>
<tr>
<td>1</td>
<td>Roof level beam soffit</td>
<td>39</td>
<td>48</td>
</tr>
<tr>
<td>2</td>
<td>Roof level slab soffit</td>
<td>42</td>
<td>47</td>
</tr>
<tr>
<td>3</td>
<td>Roof level beam soffit</td>
<td>40</td>
<td>47</td>
</tr>
<tr>
<td>4</td>
<td>Roof level secondary beam soffit</td>
<td>39</td>
<td>43</td>
</tr>
<tr>
<td>5</td>
<td>Roof level slab soffit</td>
<td>39</td>
<td>48</td>
</tr>
<tr>
<td>6</td>
<td>Roof level slab soffit</td>
<td>40</td>
<td>49</td>
</tr>
<tr>
<td>7</td>
<td>Roof level secondary beam soffit</td>
<td>38</td>
<td>42</td>
</tr>
<tr>
<td>8</td>
<td>Roof level slab soffit</td>
<td>37</td>
<td>43</td>
</tr>
<tr>
<td>9</td>
<td>Roof level beam soffit</td>
<td>35</td>
<td>45</td>
</tr>
<tr>
<td>10</td>
<td>Roof level beam soffit</td>
<td>36</td>
<td>48</td>
</tr>
<tr>
<td>11</td>
<td>3rd level top beam</td>
<td>28</td>
<td>32</td>
</tr>
<tr>
<td>12</td>
<td>3rd level top slab</td>
<td>32</td>
<td>36</td>
</tr>
<tr>
<td>13</td>
<td>3rd level top beam</td>
<td>36</td>
<td>40</td>
</tr>
<tr>
<td>14</td>
<td>3rd level top slab</td>
<td>32</td>
<td>36</td>
</tr>
<tr>
<td>15</td>
<td>3rd level top slab</td>
<td>31</td>
<td>35</td>
</tr>
<tr>
<td>16</td>
<td>3rd level top beam</td>
<td>30</td>
<td>38</td>
</tr>
<tr>
<td>17</td>
<td>3rd level top slab</td>
<td>32</td>
<td>38</td>
</tr>
<tr>
<td>18</td>
<td>3rd level top beam</td>
<td>38</td>
<td>42</td>
</tr>
</tbody>
</table>
3. CONDITION ASSESSMENT

3.1. FIELD ASSESSMENT

3.1.4. Ferroscan Pachometer Survey

- The ferroscan pachometer surveys were performed to estimate the core sample locations.
- No scans were performed on the concrete surface with exposed rebars as the core sample location can be visibly determined.
3. CONDITION ASSESSMENT

3.1. FIELD ASSESSMENT

3.1.5. Concrete Core and Steel Rebar Sample Extraction

- Fifteen (15) concrete core specimens were collected using wet rotary diamond core drilling techniques at selected locations. Concrete core samples were visually examined and photographed prior to concrete laboratory testing. Concrete core holes were patched with shrinkage-compensating repair mortar subsequent to sample collection.

- A total of nine (9) steel rebar samples were collected on site. Seven (7) samples were collected from the roof level which is grade 460 rebar, and two (2) samples (3B1 and 3B2) were collected from the 3\textsuperscript{rd} storey level which is A6BRC. The collected steel samples were sent to the accredited laboratory for further laboratory tests.
3. CONDITION ASSESSMENT

3.2. LABORATORY TEST

3.2.1. Concrete Compressive Strength Test

- Eight (8) numbers of extracted core samples were tested to determine the laboratory compressive strength. The core samples were prepared by the laboratory such that it reflected the homogeneity of the sample.
- The concrete compressive strength ranges from 30.00 to 39.00 N/mm²,

<table>
<thead>
<tr>
<th>Core sample reference</th>
<th>Location</th>
<th>Estimated in situ cube strength $f_{cu}$ (N/mm²)</th>
</tr>
</thead>
<tbody>
<tr>
<td>C1</td>
<td>3rd Floor Top Slab</td>
<td>33.00</td>
</tr>
<tr>
<td>C4</td>
<td>3rd Floor Top Slab</td>
<td>32.50</td>
</tr>
<tr>
<td>C6</td>
<td>Roof Level Beam Soffit</td>
<td>38.50</td>
</tr>
<tr>
<td>C8</td>
<td>Roof Level Slab Soffit</td>
<td>30.00</td>
</tr>
<tr>
<td>C9</td>
<td>Roof Level Beam Soffit</td>
<td>36.50</td>
</tr>
<tr>
<td>C11</td>
<td>Roof Level Beam Soffit</td>
<td>35.50</td>
</tr>
<tr>
<td>C13</td>
<td>Roof Level Slab Soffit</td>
<td>39.00</td>
</tr>
<tr>
<td>C15</td>
<td>Roof Level Beam Soffit</td>
<td>32.50</td>
</tr>
</tbody>
</table>
3. CONDITION ASSESSMENT

3.2. LABORATORY TEST

3.2.2. Petrographic Examination

- Petrographic examinations were performed on seven (7) submitted core samples to determine the extent of the concrete damage. All samples were analyzed starting from the sample surface exposed to the fire.
- Carbonation was noted within the 5mm depth.
- Some micro cracks were noted on the cement paste. Some of these were not fire-induced cracks which occurred before the fire.

(a) Under plane polarized light  (b) Under cross polarized light  (c) Under fluorescent light
### 3. CONDITION ASSESSMENT

#### 3.2. LABORATORY TEST

#### 3.2.2. Petrographic Examination

<table>
<thead>
<tr>
<th>Core sample reference</th>
<th>Location</th>
<th>Carbonation depth</th>
<th>Cement paste condition</th>
<th>Estimated exposed temperature</th>
</tr>
</thead>
<tbody>
<tr>
<td>C2</td>
<td>3rd Floor Top Slab</td>
<td>4mm</td>
<td>- Very small amount of micro cracks on cement paste were noted.</td>
<td>&lt; 300°C</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>- No Aggregate-cement paste debonding was noted</td>
<td></td>
</tr>
<tr>
<td>C3</td>
<td>3rd Floor Top Beam</td>
<td>4mm</td>
<td>- Hardened Crack with aggregate-cement paste debonding was noted at within 3mm from the exposed surface</td>
<td></td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>- No fire-induced micro cracks were noted</td>
<td>&lt; 300°C</td>
</tr>
<tr>
<td>C5</td>
<td>Roof Level Beam Soffit</td>
<td>0.5mm</td>
<td>- Hardened Crack with aggregate-cement paste debonding was noted at within 4mm from the exposed surface</td>
<td></td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>- No fire-induced micro cracks were noted</td>
<td>&lt; 450°C</td>
</tr>
<tr>
<td>C7</td>
<td>Roof Level Slab Soffit</td>
<td>2mm</td>
<td>- Hardened Crack with aggregate-cement paste debonding was noted at within 20mm from the exposed surface</td>
<td></td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>- No fire-induced micro cracks were noted</td>
<td>&lt; 450°C</td>
</tr>
</tbody>
</table>
## 3. CONDITION ASSESSMENT

### 3.2. LABORATORY TEST

#### 3.2.2. Petrographic Examination

<table>
<thead>
<tr>
<th>Core sample reference</th>
<th>Location</th>
<th>Carbonation depth</th>
<th>Cement paste condition</th>
<th>Estimated exposed temperature</th>
</tr>
</thead>
</table>
| C10                   | Roof Level Beam Soffit    | 1.5mm             | - Hardened Crack with aggregate-cement paste debonding was noted at within 20mm from the exposed surface  
- No fire-induced micro cracks were noted                                                                                                                 | < 450°C                       |
| C12                   | Roof Level Slab Soffit    | 4mm               | - Hardened Crack with aggregate-cement paste debonding was noted at within 1.5mm from the exposed surface  
- No fire-induced micro cracks were noted                                                                                                                 | < 450°C                       |
| C14                   | Roof Level Beam Soffit    | 3mm               | - Hardened Crack with aggregate-cement paste debonding was noted at within 1.5mm from the exposed surface  
- No fire-induced micro cracks were noted                                                                                                                 | < 450°C                       |
3. CONDITION ASSESSMENT

3.2. LABORATORY TEST

3.2.3. Steel Rebar Test

- The tensile test results showed that the yield strength ranged from 573.10 to 670.50 N/mm$^2$ which was more than the requirement specified in BS 4449:1997 of 460 N/mm$^2$.
- The bending test showed a satisfactory result for all the rebar samples.
- The Vickers Hardness Test showed an HV10 value range from 175 to 300, which could be correlated to estimate the tensile strength of 590 to 960 N/mm$^2$.

<table>
<thead>
<tr>
<th>Sample reference</th>
<th>Location</th>
<th>Yield strength (N/mm$^2$)</th>
<th>Bending test</th>
<th>HV10</th>
</tr>
</thead>
<tbody>
<tr>
<td>BR1</td>
<td>Roof Level Beam Soffit</td>
<td>635.00</td>
<td>Satisfactory</td>
<td>188 – 230</td>
</tr>
<tr>
<td>BR1a</td>
<td>Roof Level Slab Soffit</td>
<td>581.80</td>
<td>Satisfactory</td>
<td>188 – 237</td>
</tr>
<tr>
<td>BR2</td>
<td>Roof Level Beam Soffit</td>
<td>623.70</td>
<td>Satisfactory</td>
<td>192 – 237</td>
</tr>
<tr>
<td>BR4</td>
<td>Roof Level Beam Soffit</td>
<td>670.50</td>
<td>Satisfactory</td>
<td>192 – 300</td>
</tr>
<tr>
<td>BR5</td>
<td>Roof Level Beam Soffit</td>
<td>650.70</td>
<td>Satisfactory</td>
<td>196 – 242</td>
</tr>
<tr>
<td>BR6</td>
<td>Roof Level Slab Soffit</td>
<td>608.50</td>
<td>Satisfactory</td>
<td>194 – 219</td>
</tr>
<tr>
<td>BR7</td>
<td>Roof Level Slab Soffit</td>
<td>573.10</td>
<td>Satisfactory</td>
<td>175 – 233</td>
</tr>
<tr>
<td>3B1</td>
<td>3$^{rd}$ Floor Top Slab</td>
<td>530.70</td>
<td>Satisfactory</td>
<td>208 – 227</td>
</tr>
<tr>
<td>3B2</td>
<td>3$^{rd}$ Floor Top Beam</td>
<td>570.70</td>
<td>Satisfactory</td>
<td>215 – 218</td>
</tr>
</tbody>
</table>
3. CONDITION ASSESSMENT

3.2. LABORATORY TEST

3.2.3. Steel Rebar Test

Approximate Hardness Conversion Numbers [ASTM A370]
4. ANALYSIS

4.1. CONCRETE MATERIAL PROPERTIES

- Compressive strength results indicated that concrete strength ranged from 30.00 to 39.00 N/mm$^2$. The average laboratory compressive strength tested for eight (8) of the concrete cores extracted was 34.69 N/mm$^2$. BS1881 Part 120 allows extracted concrete core specimens subjected to laboratory compression testing to represent 95% of the design compressive strength due to the destructive nature of the core extraction process. Thus, the average residual concrete compressive strength on the site shall be 36.51 N/mm$^2$, which was slightly higher than the original design compressive strength of 35 N/mm$^2$.
- Rebound Hammer conducted on the concrete structure revealed relatively consistent concrete material properties. Testing data revealed that the concrete could be considered in a general “good” condition.
4. ANALYSIS

4.1. CONCRETE MATERIAL PROPERTIES

- No concrete delamination was noted outside the concrete spalled area as confirmed by the acoustic impact testing.
4. ANALYSIS

4.1. CONCRETE MATERIAL PROPERTIES

- Petrographic examination showed that all tested core samples had some carbonation that occurred at a depth of 5mm below the exposed surface. At the location where concrete spalled exposing steel rebar, the exposed surface was deeper than the steel rebar depth. Hence, concrete material carbonation might be a significant contributor to the steel rebar corrosion in the future. However, in the location where there was no concrete spalling, the 5mm deep carbonation was well within the concrete cover, thus carbonation would not have a significant impact on rebar corrosion.
4. ANALYSIS

4.1. CONCRETE MATERIAL PROPERTIES

• Some micro cracks were noted inside the cement paste within 20mm from the exposed surface. Some of these micro cracks were existing cracks which occurred before the fire whereas some were fire-induced. Some aggregate-cement paste debonding was observed on the existing micro cracks within 20mm from the exposed surface. However, no cracks were observed on the aggregates. The concrete at the depth of more than 20mm was considered to be in good condition as no signs of distress were observed.

• Petrographic examination suggested that the top 5mm of the concrete surface might be exposed to a temperature not more than 450°C. The remaining depth of the concrete was strongly believed to be exposed to a temperature of less than 300°C.
4. ANALYSIS

4.2. STEEL MATERIAL PROPERTIES

- All three tests (tensile, bending, and hardness) on the steel samples showed that the steel rebars were still in good condition with no significant material degradations caused by the fire incident.

- All post tension strands were encased inside fully grouted corrugated steel ducts. In order for the fire to damage the strands, the heat needed to go through the 70mm thick concrete cover, steel duct, and about 30mm-thick grout. After the fire incident, no tendons were exposed even at the most severely spalled concrete. This showed that the strands were still in good condition.

- Thus, it could be concluded that the steel rebars and PT strands were considered to be structurally able to perform as designed.
5. CONCLUSION

- A comprehensive condition assessment is a very important work to determine the extent of structural damage and the residual material mechanical properties.
- The findings of this assessment were used for the structural assessment work to determine the residual structural capacity of the affected structural elements.
- The effective structural rehabilitations, which includes structural repair and strengthening works, were done based on the findings of both condition and structural assessment works, respectively.
THANK YOU